

Online supplementary material for

Outburst floods of the Maly Yenisei. Part I – Review

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Sensitivity of ^{10}Be age calculations to the scaling schemes

The published ^{10}Be ages were recalculated using CRONUS-Earth version 2.2 (Balco *et al.* 2008) with the globally calibrated ^{10}Be production rate of 3.99 ± 0.22 atoms $\text{g}^{-1} \text{yr}^{-1}$ (Heyman 2014) when referenced to the scaling of Stone (2000). Gillespie *et al.* (2008) used CRONUS-Earth version 1.2 with a production rate of 5.2 atoms $\text{g}^{-1} \text{yr}^{-1}$ and adopted the scaling of Lal (1991) and corrected for paleomagnetic variation, which is called Lm in Table S1. Arzhannikov *et al.* (2012) reported using the production rate of 4.49 ± 0.29 atoms $\text{g}^{-1} \text{yr}^{-1}$; Rother *et al.* (2014) used 4.43 ± 0.52 atoms $\text{g}^{-1} \text{yr}^{-1}$ referenced to Dunai scaling (Dunai 2001). For consistency we accepted only the ages with the scaling of Stone (2000) without paleomagnetic correction, because the total 1σ uncertainty of the ages from the other scaling schemes did not exceed the margin of analytical error. In the recalculation we used 2.7 g cm^{-3} for sample density (same value used in Gillespie *et al.* 2008), instead of 2.5 g cm^{-3} in Arzhannikov *et al.* (2012) and 2.6 g cm^{-3} in Rother *et al.* (2014). Using 2.6 g cm^{-3} would make less than 0.3% difference in the apparent age for samples <10 cm thick. No burial history and zero erosion were assumed in the recalculation of the ^{10}Be ages.

Table S1. ^{10}Be exposure ages (in $\text{ka} \pm 1\sigma$) for all the samples summarized in Figure 10 in the main text calculated using various scaling schemes for spallation. St: Lal (1991)/Stone (2000); De: Desilets *et al.* (2003, 2006); Du: Dunai (2001); Li: Lifton *et al.* (2005); Lm: Time-dependent Lal (1991)/Stone (2000). The ages shown in bold (St) are discussed in the text.

Sample ID	St	De	Du	Li	Lm
Darhad basin group (from Gillespie <i>et al.</i> 2008)					
081400-arg-Tin-01	21.3 ± 1.3	21.6 ± 1.7	21.8 ± 1.6	21.1 ± 1.5	21.5 ± 1.2
081400-arg-Tin-01b	23.9 ± 1.5	24.2 ± 1.9	24.4 ± 1.8	23.7 ± 1.6	24.1 ± 1.4
081700-rmb-Tin-01a	34.6 ± 2.2	34.8 ± 2.7	34.9 ± 2.6	33.7 ± 2.4	34.7 ± 2.0
081700-rmb-Tin-01c	28.0 ± 1.7	28.3 ± 2.2	28.4 ± 2.1	27.5 ± 1.9	28.2 ± 1.6
081700-arg-Uzg-002d	16.8 ± 1.1	16.9 ± 1.4	17.1 ± 1.3	16.6 ± 1.2	17.0 ± 1.0
081700-arg-Uzg-003	30.5 ± 2.0	30.5 ± 2.4	30.6 ± 2.3	29.5 ± 2.1	30.6 ± 1.8
080900-arg-Gar-Ia-001	23.7 ± 1.5	24.1 ± 1.8	24.3 ± 1.8	23.5 ± 1.6	23.9 ± 1.4
080900-arg-Gar-Ia-002	21.1 ± 1.3	21.5 ± 1.6	21.6 ± 1.6	21.0 ± 1.5	21.3 ± 1.2
081000-arg-Gar-Ia-003	25.1 ± 1.5	25.5 ± 1.9	25.6 ± 1.9	24.8 ± 1.7	25.3 ± 1.4
081000-arg-Gar-Ia-010	45.4 ± 2.7	45.9 ± 3.4	45.9 ± 3.4	44.4 ± 3.0	45.4 ± 2.5
081000-arg-Gar-Ia-011	44.7 ± 4.1	45.1 ± 4.5	45.2 ± 4.4	43.7 ± 4.1	44.7 ± 3.8
081000-arg-Gar-Ia-012	19.5 ± 1.2	19.8 ± 1.5	20.0 ± 1.5	19.4 ± 1.3	19.7 ± 1.1
081000-arg-Gar-Ia-013	20.3 ± 1.3	20.7 ± 1.6	20.8 ± 1.6	20.2 ± 1.4	20.5 ± 1.2
081000-arg-Gar-IIa-005	30.4 ± 1.9	30.8 ± 2.4	30.9 ± 2.3	29.9 ± 2.1	30.6 ± 1.7
081000-arg-Gar-IIa-007	18.6 ± 1.1	18.9 ± 1.4	19.0 ± 1.4	18.5 ± 1.3	18.8 ± 1.1
081000-arg-Gar-IIa-008	21.4 ± 1.3	21.7 ± 1.6	21.9 ± 1.6	21.2 ± 1.4	21.6 ± 1.2
082100-arg-Huj-01a	246.9 ± 19.2	247.2 ± 22.2	247.4 ± 21.6	237.5 ± 19.7	246.4 ± 17.5
082100-arg-Huj-01b	111.9 ± 6.7	112.2 ± 8.6	112.3 ± 8.3	108.1 ± 7.5	111.7 ± 6.2
082100-arg-Huj-01c	142.8 ± 8.6	143.1 ± 11.0	143.1 ± 10.6	137.6 ± 9.6	142.4 ± 7.9
082100-arg-Huj-02c	16.5 ± 1.1	16.8 ± 1.3	16.9 ± 1.3	16.5 ± 1.2	16.6 ± 1.0
082100-arg-Huj-02d	45.3 ± 2.8	45.6 ± 3.5	45.7 ± 3.4	44.2 ± 3.1	45.3 ± 2.6
082100-arg-Huj-02e	29.1 ± 1.9	29.4 ± 2.3	29.6 ± 2.3	28.6 ± 2.1	29.2 ± 1.8
East Sayan mountains group (from Arzhannikov <i>et al.</i> 2012)					
S07BE6	18.2 ± 3.2	18.6 ± 3.4	18.7 ± 3.4	18.2 ± 3.3	18.3 ± 3.2
S07BE7	20.6 ± 1.4	21.1 ± 1.7	21.2 ± 1.7	20.6 ± 1.5	20.8 ± 1.3
S07BE8	18.1 ± 1.5	18.5 ± 1.8	18.6 ± 1.7	18.1 ± 1.6	18.2 ± 1.5
S07BE9	17.4 ± 1.3	17.8 ± 1.6	17.9 ± 1.6	17.4 ± 1.5	17.5 ± 1.3
S07BE10	26.4 ± 1.9	27.1 ± 2.4	27.2 ± 2.3	26.4 ± 2.1	26.6 ± 1.9
S07BE11	24.3 ± 1.8	24.9 ± 2.2	25.1 ± 2.1	24.3 ± 2.0	24.5 ± 1.7
S07BE12	25.1 ± 2.9	25.7 ± 3.2	25.9 ± 3.1	25.1 ± 3.0	25.3 ± 2.8
S07BE13	27.1 ± 1.9	27.7 ± 2.4	27.8 ± 2.3	26.9 ± 2.1	27.2 ± 1.8
S07BE14	26.0 ± 2.5	26.6 ± 2.9	26.7 ± 2.8	25.9 ± 2.7	26.2 ± 2.5
S07BE15	44.5 ± 3.6	45.4 ± 4.3	45.4 ± 4.2	43.9 ± 3.9	44.6 ± 3.5
S07BE16	70.4 ± 5.7	71.8 ± 6.7	71.8 ± 6.6	69.4 ± 6.1	70.5 ± 5.5
S07BE17	17.0 ± 1.4	17.5 ± 1.6	17.6 ± 1.6	17.1 ± 1.5	17.2 ± 1.3
S07BE18	18.1 ± 1.6	18.5 ± 1.9	18.7 ± 1.8	18.1 ± 1.7	18.2 ± 1.6

Table S1 (continued).

Sample ID	St	De	Du	Li	Lm
Otgontenger mountain group (from Rother <i>et al.</i> 2014)					
MON-D-II-I	16.6 ± 1.0	16.6 ± 1.3	16.7 ± 1.2	16.5 ± 1.2	16.6 ± 1.0
MON-D-II-II	16.5 ± 1.0	16.4 ± 1.3	16.6 ± 1.2	16.3 ± 1.1	16.5 ± 0.9
MON-D-II-III	33.5 ± 2.0	32.6 ± 2.5	32.8 ± 2.4	32.0 ± 2.2	32.9 ± 1.9
MON-D-IV-I	21.6 ± 1.3	21.3 ± 1.6	21.4 ± 1.6	21.0 ± 1.5	21.5 ± 1.2
MON-D-IV-II	18.7 ± 1.2	18.5 ± 1.4	18.7 ± 1.4	18.3 ± 1.3	18.6 ± 1.1
MON-D-IV-III	15.0 ± 0.9	14.9 ± 1.2	15.1 ± 1.2	14.9 ± 1.1	15.0 ± 0.9
MON-F-I-I	26.8 ± 1.7	26.0 ± 2.0	26.2 ± 2.0	25.6 ± 1.8	26.4 ± 1.5
MON-F-I-II	28.5 ± 1.8	27.6 ± 2.1	27.7 ± 2.1	27.1 ± 1.9	28.1 ± 1.6
MON-F-I-IV	23.4 ± 1.4	22.8 ± 1.8	22.9 ± 1.7	22.5 ± 1.6	23.2 ± 1.3
MON-E-III-I	19.2 ± 1.2	18.8 ± 1.5	19.0 ± 1.4	18.6 ± 1.3	19.1 ± 1.1
MON-E-III-II	18.9 ± 1.2	18.5 ± 1.5	18.7 ± 1.4	18.4 ± 1.3	18.8 ± 1.1
MON-E-III-III	18.6 ± 1.1	18.2 ± 1.4	18.4 ± 1.4	18.1 ± 1.3	18.5 ± 1.1
MON-D-I-I	45.1 ± 2.8	43.4 ± 3.3	43.6 ± 3.2	42.3 ± 3.0	44.0 ± 2.5
MON-D-I-II	22.4 ± 1.4	22.0 ± 1.7	22.2 ± 1.6	21.8 ± 1.5	22.2 ± 1.3
MON-D-I-III	41.9 ± 2.6	40.4 ± 3.1	40.6 ± 3.0	39.5 ± 2.8	41.0 ± 2.3
MON-E-I-I	42.9 ± 2.6	40.3 ± 3.1	40.5 ± 3.0	39.2 ± 2.8	41.9 ± 2.4
MON-E-I-II	59.5 ± 3.6	55.8 ± 4.3	55.9 ± 4.2	54.1 ± 3.8	58.1 ± 3.3
MON-E-I-III	31.9 ± 2.4	30.3 ± 2.7	30.4 ± 2.6	29.6 ± 2.5	31.4 ± 2.3
MON-E-II-I	63.5 ± 4.0	59.6 ± 4.7	59.7 ± 4.5	57.9 ± 4.2	62.1 ± 3.7
MON-E-II-II	23.6 ± 1.5	22.6 ± 1.7	22.7 ± 1.7	22.2 ± 1.6	23.4 ± 1.4
MON-E-II-III	40.1 ± 2.5	37.6 ± 2.9	37.8 ± 2.8	36.7 ± 2.6	39.2 ± 2.2

Calculation of bed shear stress and the size of mobilized particles

Komatsu *et al.* (2009) estimated that the peak discharge rate of an instant flood from a 172 m deep Darhad lake would reach $\sim 3.5 \times 10^6 \text{ m}^3 \text{ s}^{-1}$ and rapidly decrease to $\sim 0.5 \times 10^6 \text{ m}^3 \text{ s}^{-1}$ after ~ 20 hours. We used the range of peak discharges of Komatsu *et al.* (2009) and calculated the bed shear stress on the Maly Yenisei gorge immediately upstream the Tengis glacier. Then, using the bed shear stress we calculated the maximum size of particles (with average rock density of 2700 kg m^{-3}) that could be mobilized in the flood. The approach is detailed below:

Table S2. Parameters used for the calculation of bed shear stress and size of particles mobilized.

Parameter, symbol	Values used [unit]
Peak discharge, Q	$0.5 - 3.5 [10^6 \text{ m}^3 \text{ s}^{-1}]$
Bed roughness length scale, k_s	$0.1 - 1 [\text{m}]$
Hillslope angle, φ	$10 [\text{degrees}]$
Mean bed slope, S	0.027
Average rock density, ρ_s	$2700 [\text{kg m}^3]$
Water density, ρ	$1000 [\text{kg m}^3]$
Kinematic viscosity at 20°C , ν	$1 \times 10^{-6} [\text{m}^2 \text{ s}^{-1}]$
Flow depth, h	$170 [\text{m}]$
Width of the valley floor, w	$700 [\text{m}]$
Acceleration due gravity, g	$9.81 [\text{m s}^{-2}]$

We used the equation of Lamb and Fonstad (2010) and solved for the bed shear stress:

$$Q = 8.1A \left(\frac{\tau_b}{\rho} \right)^{\frac{1}{2}} \left(\frac{h}{k_s} \right)^{\frac{1}{6}} \quad (1)$$

where h is the flow depth and A is the cross sectional area of the flow, calculated from an approximated trapezoid valley:

$$A = hw + \tan \varphi h^2 \quad (2)$$

where w is the width of the flat bottom.

Using the τ_b we solve for the intermediate axis length of a median block size \overline{D}_2 using the relation:

$$\overline{D}_2 = \frac{\tau_b}{\tau_{*C}g(\rho_s-\rho)} \quad (3)$$

where the critical stress for insipient motion, τ_{*C} , was estimated from Lamb *et al.* (2008) and references therein:

$$\tau_{*C} = 0.15S^{0.25} \quad (4)$$

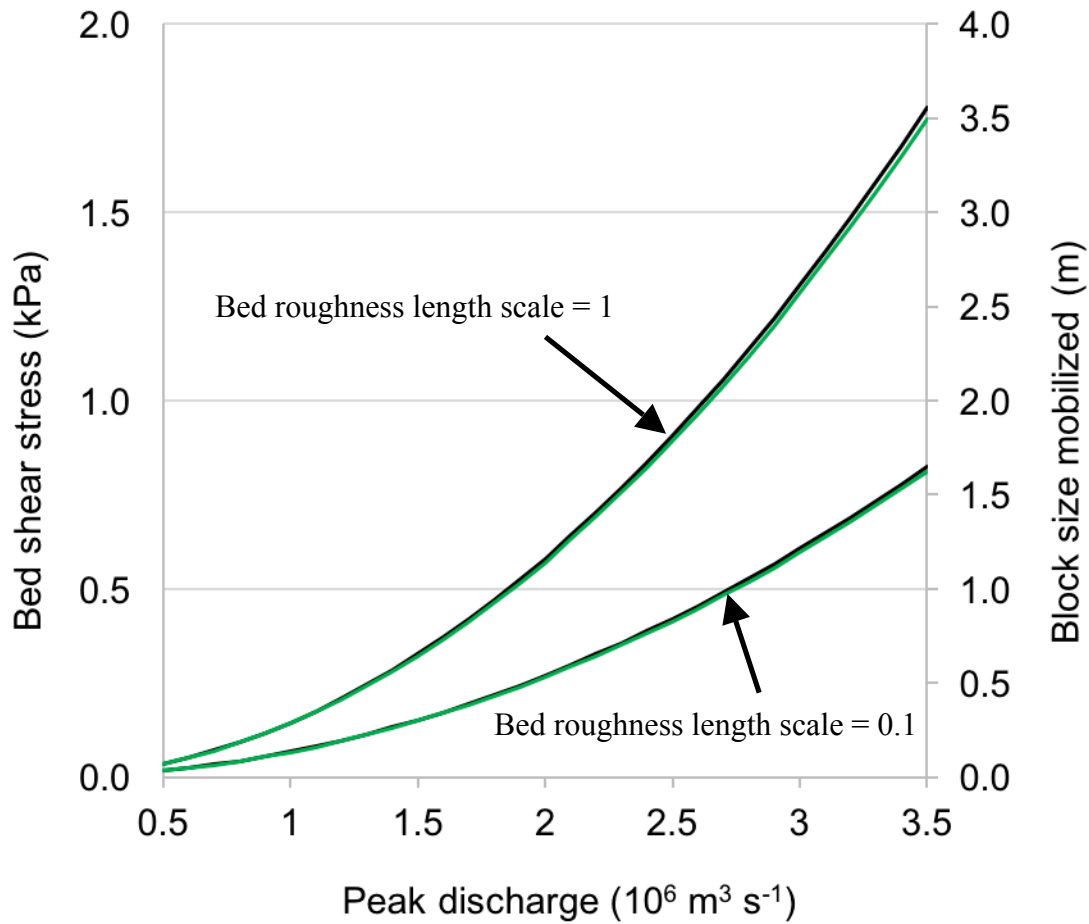


Figure S1. Calculated bed shear stress and maximum particle size mobilized in a water flow with various peak discharge through a 700-m wide gorge. The calculated values are sensitive to and directly related with the bed roughness length scale (ranging 0.1 to 1 m).

The black curves are for bed shear stress, and the green curves are for block size.

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